# APPENDIX 4-2

***PEAT AND SPOIL MANAGEMENT PLAN***

FEHILY TIMONEY

DESIGNING AND DELIVERING
A SUSTAINABLE FUTURE

# MEENBOG WIND FARM (PROSPECTIVE DEVELOPMENT)

## PEAT AND SPOIL MANAGEMENT PLAN

Prepared for: **MKO Ltd**

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# PEAT AND SPOIL MANAGEMENT PLAN
# MEENBOG WIND FARM (PROSPECTIVE DEVELOPMENT)

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**Abstract:** Fehily Timoney and Company (FT) were engaged by MKO Ltd. to compile a Peat and Spoil Management Plan (PSMP) for the Meenbog Wind Farm Site. The purpose of this report is to provide a Peat and Spoil Management Plan for the construction phase of the Prospective Development. The report describes how peat and spoil which will be excavated from infrastructure locations such as turbine bases and roads and will be handled and placed/reinstated onsite. The report also provides construction details for the types of roads which will be put in place at the Wind Farm Site and BMEP Site and proposed peat and spoil placement/reinstatement areas which will be developed at the Wind Farm Site.

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# 1. INTRODUCTION

## 1.1 Fehily Timoney and Company

Fehily Timoney and Company (FT) is an Irish engineering, environmental science and planning consultancy with offices in Cork, Dublin and Carlow. The practice was established in 1990 and currently has c.100 members of staff, including engineers, scientists, planners and technical support staff. We deliver projects in Ireland and internationally in our core competency areas of Waste Management, Environment and Energy, Civils Infrastructure, Planning and GIS and Data Management.

This Report was written by Ian Higgins (FT Technical Director, PGeo, MSc in Geotechnical Engineering). Ian is a Technical Director with Fehily Timoney and has over 25 years' experience in geotechnical engineering.

## 1.2 Project Description

Fehily Timoney and Company (FT) was engaged by MKO Ltd. to compile a Peat and Spoil Management Plan for the works to be carried out at the Wind Farm Site and the BMEP Site as part of the Prospective Development..

The substitute consent application seeks to regularise the Existing Development and seeks permission for the Prospective Development. The Prospective Development is addressed within this Environmental Impact Assessment Report (EIAR). The Existing Development is addressed within the remedial Environmental Impact Assessment Report (rEIAR), which accompanies this planning application.

The 'Site' refers to the Wind Farm Site, Grid Connection Site, and BMEP (Biodiversity Management and Enhancement Site) Site combined.

As detailed in Section 1.1.1 in Chapter 1 of the EIAR, the various development components are described and assessed using the following references: 'Subject Development', 'Existing Development','Prospective Development', 'Permitted Development', 'Site', 'Wind Farm Site', 'Grid Connection Site', 'BMEP Site', 'Grid Connection', ' November 2020 Peat Slide', '2017 EIAR' and 'proposed turbines' or 'proposed turbine locations'.

The Wind Farm Site is located approximately 8km southwest of the twin towns of Ballybofey and Stranorlar and 12km northeast of Donegal Town.

The land use at the Wind Farm Site comprises predominantly forestry. The surrounding landscape is rolling hillsides with land-use comprising forestry and blanket peatland.

The Prospective Development will comprise the following:

- 19 no. wind turbines, with an overall tip height of 156.5m, rotor diameter of 133m, and wind turbine hub height of 90m, and 1 no. meteorological mast with a height of 80m, and subsequent decommissioning of the wind turbines and meteorological mast, following a twenty five-year operational period from the date of full commissioning of the wind farm;

- The completion of upgraded access junctions, tracks and roads, and construction of new site access roads;
- The completion of construction of all 19 no. wind turbine foundations and hardstand areas, and the construction of a meteorological mast foundation;
- Completion of internal wind farm underground ducting and cabling;
- Continued use of and upgrade of 2no. temporary construction compounds;
- Continued use and extraction at the 3no. borrow pits;
- Peat and spoil management, including site landscaping;
- Forestry felling;
- Site drainage and sediment control measures;
- Biodiversity enhancement measures (including peatland habitat restoration and Hen Harrier habitat areas);
- Recreation and amenity works (including carpark, play, picnic & amenity areas and pedestrian access paths to the wind farm roads);
- Operational stage site signage; and
- All associated site development works.

## 1.3 Purpose

The purpose of this report is to provide a peat and spoil management plan with particular reference to peat stability for the construction phase of the Prospective Development. The report describes how peat and spoil which will be excavated from infrastructure locations such as turbine bases, hardstands and roads will be handled and placed/reinstated onsite. The report also provides construction details for the types of roads which will be put in place at the Wind Farm Site and proposed peat and spoil management areas which will be developed at the Wind Farm Site.

This peat and spoil management plan also includes a monitoring programme which will be implemented during the construction phase of the Prospective Development and a contingency plan should peat instability/failure occur at the Wind Farm Site.

As work is carried out on the Site the contents of the peat and spoil management plan and peat stability monitoring programme will be implemented in full and updated (if required) in the Construction & Environmental Management Plan (CEMP) for the construction phase.

This peat and spoil management plan contains some drainage guidelines for construction works and for management of peat on the Site. It should be noted that the control of water quality and drainage measures for the Wind Farm Site is outlined in detail in Chapter 4: Description of the Prospective Development and Chapter 9: Water of the Environmental Impact Assessment Report (EIAR).

## 1.4 Peat Instability Definition

Peat instability in this report is defined as a mass movement of a body of peat that would have a significant adverse impact on the surrounding environment. Peat instability excludes localised movement of peat that would occur below a floating access road, creep movement or localised erosion type events.

Adherence to the Peat and Spoil Management Plan (PSMP) should reasonably minimise the potential for all such peat movements during construction works. However, it is noted that due to the soft ground nature of the peat terrain it is not possible to completely avoid such localised peat movement as described above.

## 1.5 Ground Conditions

Ground conditions across the Wind Farm Site are described in the Geotechnical & Peat Stability Assessment Report (Prospective Development) (FT, 2026).

The general sequence of ground conditions at the Site is summarised as follows:

(1) Blanket peat. Extensive covering of blanket peat, with peat depth typically in the range of 0.5 to 2m, though locally variable with areas of shallower and deeper peat (measured maximum depth of 7.3m).

(2) Mineral soil or weathered rock. Underlying the blanket peat was a thin mineral subsoil layer recorded as 0.1 to 0.45m thick of likely glacial till or weathered bedrock, or locally normally consolidated mineral subsoil, which may have been deposited in a lacustrine environment.

(3) Bedrock. Generally, bedrock at shallow depth either directly underlying the blanket peat or underlying the mineral soil/weathered rock layer. Bedrock is described as a strong to very strong thinly foliated fine and medium grained Phyllite with medium spaced (locally closely spaced) discontinuities.

## 1.6 Relevant Guidance

The relevant guidance used and referred to throughout this report includes;

- Geological Survey of Ireland (DCEE)/National Parks and Wildlife (DHLGH), 2024. Assessment of main contributing factors leading to three major peatland failures in Leitrim, Kerry and Donegal.
- Good Practice during Windfarm Construction (NatureScot, 2024);
- Guidance on Developments on Peatland: Site Surveys (Scottish Government, Scottish Natural Heritage and SEPA, 2017;
- Munro, R, 2004. Dealing with bearing capacity problems on low volume roads constructed on peat. Roadex II Northern Periphery;
- Scottish Natural Heritage/Forestry Commission Scotland, 2010. Floating Roads on Peat;
- Scottish Natural Heritage, 2015. Constructed Tracks in the Scottish Uplands. Scottish Natural Heritage.

# 2. CONSTRUCTION ACTIVITIES COVERED BY PEAT AND SPOIL MANAGEMENT PLAN

## 2.1 Construction Activities

For the construction phase of the Prospective Development the activities that will generate peat and spoil are as follows:

(1) Upgrade of existing floating access roads (as excavate and replace roads)

(2) Widening of existing excavated roads through peat

(3) Excavation and placement of arisings

(4) Excavations in peat and overburden for borrow pits

(5) Excavations in peat for turbine bases, hardstands and other infrastructure foundations

(6) Excavations for underground cables

Peat and spoil management of the above construction activities are covered individually in this report.

## 2.2 Road Construction Types

To provide access within the Wind Farm Site, the BMEP Site and to connect the proposed turbines and associated infrastructure existing roads will need to be upgraded and new roads constructed. These have been classified as 'Roads – Minor Works and Upgrades' (majority of the Wind Farm Site) and 'Roads – More Substantial Works and Upgrades' (generally localised, with the exception of the upgrade of the road to T18).

The road construction preliminary design has taken into account the following key factors:

(1) Buildability considerations

(2) Maximising use of existing infrastructure

(3) Minimising excavation arisings

(4) Peat stability

(5) Serviceability requirements for construction and wind turbine delivery and maintenance vehicles

(6) Requirement to minimise disruption to peat hydrology

Whilst the above key factors are used to determine the road design the actual construction technique employed for a particular length of road will be determined by the prevailing ground conditions encountered along that length of road.

The general road construction techniques to be considered are given in Table 2.1.

This report includes the most suitable type of road construction envisaged for each section of access road based on the ground/site conditions recorded during the site walkovers and intrusive site investigation works. The design of these roads is discussed in the FT Report "Meenbog Wind Farm (Peat Stabilisation Works)" (P25160-FT-EGT-XX-RP-GE-0001).

No new floating access roads are proposed within the Wind Farm Site, however some of the previously constructed floating roads will be used in the construction of the Prospective Development within both the Wind Farm Site and the BMEP Site. A section of new floating access track is proposed to provide access to one location within the BMEP Site. The types of roads to be constructed across the Wind Farm Site are based on available guidance, including 'Constructed Tracks in the Scottish Uplands (Scottish Natural Heritage, 2nd Edition ,2015), Floating Roads on Peat (Scottish Natural Heritage/Forestry Commission Scotland, 2010) and 'Dealing with Bearing Capacity Problems on Low Volume Roads Constructed on Peat (ROADEX II, 2004).

**Table 2.1: General Road Construction Techniques**

| Construction Method | Typical Site Conditions | | | Comment |
|---|---|---|---|---|
| | Construction Type | Typical Peat Depth (m) | Typical Slope Inclination (degs) | |
| Upgrade of existing founded access roads | Type A | <1.0m, locally up to 2.6m along the road to T18 | Varies | Upgrade existing founded access roads to the required width and finished with a layer of selected granular fill – Drawing P24-234-0602-0002. |
| Upgrade/replacement of existing floated access road to founded road | Type B | Typically, less than 2.0m, locally up to 5.0m | Varies | Upgrade existing floated access roads to a founded construction the required width and finished with a layer of selected granular fill – Drawing P24-234-0602-0003. |
| Upgrade of existing floated forestry track | Type B1 | <2.0m | <5 degrees | Upgrade existing floated forestry track to provide access within the BMEP Site. Drawing P24-234-0602-0004. |
| Upgrade of existing floated access road | Type C | Typically, less than 2.0m, locally up to 7.3m | <5 degrees | Top up the existing floating roads within the Wind Farm Site to turbines T01, T02, T03 and T04 with a layer of selected granular fill. |
| New floating forestry access track | Type D | <1.5m | <5 degrees | To provide access to a single location within the BMEP. Drawing P24-234-0602-0005. |

Further details on access road construction types A to D are given in Section 3 of this report. Please note, road types A to D contain some overlap between 'Roads-Minor Works and Upgrades' and 'Roads - More Substantial Works & Upgrades' as described in Chapter 4 of the EIAR.

# 3. ACCESS ROAD CONSTRUCTION DETAILS

Approximately 19 km of existing access roads are present across the Wind Farm Site and have been in operation for a number of years. The existing access roads have been constructed using both founded and floating construction techniques. Upgrade works will involve the widening of the existing founded access roads, upgrade to existing floating roads and the construction of a short section of new floating road. The proposed locations for upgrade of the existing access roads on the Wind Farm Site are shown in Drawing P24-234-0602-0001.

The following confirmation testing and assessment will be carried out immediately in advance of construction. The confirmation testing and assessment is in addition to that already carried out across the Wind Farm Site.

(1) In advance of any remaining work associated with the access roads, a zone of influence extending 50m minimum in all directions from the proposed works area will be re-inspected and assessed by a competent person in advance of any works.

(2) Where deemed necessary by the competent person, the zone of influence will be extended to include any ground that is considered to be affected by the works.

(3) The assessment within the zone of influence will include visual inspection and appropriate testing of in-situ peat with respect to depth and strength to full peat depth. The assessment will include but not be limited to recording morphology, vegetation cover, drainage, proximity of drains and natural watercourses. The results of the assessment will be considered by the designer.

(4) The further confirmatory testing of in-situ peat with respect to depth and strength to full peat depth will comprise the following within the zone of influence and will be carried out immediately in advance of works commencing:

  (a) Peat depth determined at typically at 20m spacing using peat probes or alternatively using continuous depth profiling such as ground penetrating radar (GPR).

  (b) In-situ shear vane testing, or similar technique that measures the operational shear strength of the peat, typically at 20m spacing depending on the encountered peat condition. Testing also to be undertaken below the sections of floating road to be used as part of the Prospective Development. The use of the Geonor H10 field vane is recommended for this.

  (c) Spacing of probes and in-situ shear vane testing, or similar, to be reduced where areas of deeper peat are encountered.

(5) A hydrological assessment carried out by appropriate experienced and competent person, which will include but not be limited to drainage, proximity of drains and natural watercourses, will be carried out in advance of construction works.

(6) The results of the assessment, pending satisfactory findings, will be completed prior to any works commencing. Works will only commence following a permit to work being issued.

(7) A record of all such assessments will be maintained.

## 3.1 Upgrading Existing Founded Access Roads (Type A) Construction Methodology

This methodology includes procedures that will be included in the construction to minimise any adverse impact on peat stability. The methodology is not intended to cover all aspects of construction such as drainage and environmental considerations, which are discussed separately in Chapter 4 and 9 of the EIAR.

(1) Access road construction will be to the line and level requirements as per design/planning conditions.

(2) For upgrading of all existing founded access roads (Type A – Drawing P24-234-0602-0002) the following will apply:

(a) Excavation of the access road will take place to a competent stratum beneath the peat, removing all peat and soft clay and backfilled with suitable granular fill.

(b) Benching of the excavation will be required between the existing section of access road and the widened section of access road where the depth of excavation exceeds 500mm.

(c) Access roads will be finished with a layer of capping/surfacing material across the full width of the road.

(d) For excavations in peat, side slopes will be not greater than 1 (v): 3 (h). This slope inclination will be reviewed during construction, as appropriate. Where areas of weaker peat are encountered then slacker slopes will be required to ensure stability.

## 3.2 Upgrade of Existing Floating Access Roads to Founded (Type B) Construction Methodology

As part of the Prospective Development, sections of existing floating access roads will be upgraded to founded roads. These are described below.

A section of the existing floating access road to T04 (comprising the final 210m to the hardstand), as well as the section of existing floating access road to T07 will be excavated and replaced with a founded road. The existing floating forestry road to T18 will be excavated and replaced with a founded road. For the locations around the section of floating road at the T01 and T02/T04 junction, a stabilising berm will be constructed downslope of the road to act as a mitigation measure to provide additional resistance to peat movement, as described in the Peat Stability Assessment Report, Meenbog Wind Farm (Prospective Development), FT (2026). Monitoring posts will be installed upslope and downslope of this area prior to construction works commencing, as detailed in Section 7.

(1) For upgrading of existing floating access roads previously constructed using a floated construction technique (Type B – Drawing P24-234-0602-0003) the following will apply:

(a) Prior to commencing road construction movement monitoring posts will be installed in areas where the peat depth is greater than 2m and will be placed at 10m intervals along these sections. Daily monitoring of these monitoring posts will be undertaken while works are ongoing in specific areas.

(b) The existing floating roads will be incrementally removed by pulling back the engineering fill material and base layer, before constructing the new road using the excavate and replace/partial displacement method.

(c) The roads will be built incrementally, with peat removed before being backfilled with coarse rock sourced from the borrow pit where the peat is relatively shallow (<2m). The lateral extent of excavation will be limited to 3m (effective reach of an excavator) before being backfilled. The excavator will work from the road at all times and will not track or operate directly on the peat surface.

(d) Rock fill from the borrow pit will be transported to the roads and berm using A25 dumpers, with the coarse rock tipped onto the constructed section of road before being used to backfill the excavation. Rock will not be end tipped directly from dumpers into the excavation.

(e) Where areas of deeper or weaker peat are encountered , the partial displacement method is proposed. This removes the peat down to the stable depth of excavation but will leave a layer of peat in place at the base of the excavation.

(f) Coarse boulders (>0.5m, with no fine material) will be used in the base of the excavation and will be pushed into the base of the weaker peat to the solid stratum below the peat. This displaces the peat upwards, filling the voids between the coarse boulder fill.

(2) The finished road will have a minimum running width of 5m, with wider sections on bends and corners.

(3) The construction of access roads in areas of deep peat (greater than 3m) will be inspected on a daily basis (by the Site Manager/Ecological Clerk of Works/Project Geotechnical Engineer) during the works, particularly before/following trafficking by heavy vehicular loads.

## 3.3 Upgrade of Existing Floating Forestry Access Track (Type B1) Construction Methodology

A single section of floating forestry access track on the BMEP Site will be widened and upgraded as a floating road to allow for forestry felling operations. The proposed location is shown on drawing P24-234-0602-0001 and details shown on drawing P24-234-0602-0004. The existing track comprises coarse crushed rock fill on a layer of tree brash. Peat depth in this area is less than 2m and the slope angle is less than 5 degrees. Monitoring posts will be installed upslope and downslope of this area prior to construction works commencing, as detailed in Section 7. Peat probing and hand shear vanes testing will also be undertaken in advance of construction works commencing.

(1) Prior to commencing floating access road construction movement monitoring posts will be installed and will be placed at 10m intervals along this track.

(2) The surface of the existing access road will be scraped back to a depth of 250mm, and a layer of geogrid placed across the existing road and the widened section of the road.

(3) The existing section of road will be overlain with a 150mm layer of selected granular fill.

(4) The basal geogrid on the widened section will be overlaid with an average of 800mm of selected granular fill.

(5) The finished road width will be approximately 4m, with wider sections on bends.

(6) Additional geogrid and granular fill may be required in certain sections of the works, such as where excessive rutting is noted in the existing road.

(7) Stone delivered to the floating road construction will be end-tipped onto the constructed floating road. Direct tipping of stone onto the peat will not be carried out.

(8) To avoid excessive impact loading on the peat due to concentrated end-tipping all stone delivered to the floating road will be tipped over at least a 10m length of constructed floating road.

(9) Following end-tipping suitable machinery will be employed to spread and place the tipped stone over the base geogrid along the line of the road.

## 3.4 Upgrading Floating Access Roads (Type C) Construction Methodology

The existing floating access roads to T01, T02, T03 and T04 will be used for the construction of the Prospective Development. In these locations the existing roads will be 'topped up' with a thin layer of crushed rock, up to 150mm in thickness finished with a layer of selected granular fill. Monitoring posts will be installed upslope and downslope of this area prior to construction works commencing, as detailed in Section 7.

(1) Prior to any upgrading works, peat probing, hand shear vane testing and full-scale proof load testing will be carried out along each of the existing floating roads. See 'Geotechnical and Peat Stability Report, Meenbog Wind Farm (Prospective Development), FT (2026) for details.

(2) Prior to commencing upgrade works movement monitoring posts will be installed in areas where the peat depth is greater than 2m and will be placed at 10m intervals along these sections.

(3) The surface of the existing access road will be graded/tidied up prior to the placement any additional material.

(4) Stone delivered to the floating road construction will be end-tipped onto the constructed floating road. To avoid excessive impact loading on the peat due to concentrated end-tipping all stone delivered to the floating road will be tipped over at least a 10m length of constructed floating road.

(5) The construction of these access roads will be inspected on a daily basis (by the Site Manager/Ecological Clerk of Works/Project Geotechnical Engineer) during the works, particularly before/following trafficking by heavy vehicular loads.

## 3.5 New Floating Forestry Access Track (Type D) Construction Methodology

A new floating forestry access track, 550m in length, will be constructed in a single area on the BMEP Site. The proposed location is shown on drawing P24-234-0602-0001 and details are shown on drawing P24-234-0602-0005. Peat depth in this this area is less than 2m and the slope angle is less than 5 degrees. Monitoring posts will be installed upslope and downslope of this area prior to construction works commencing, as detailed in Section 7.

This methodology includes procedures that are to be included in the construction to minimise any adverse impact on peat stability. The methodology is not intended to cover all aspects of construction such as drainage and environmental considerations, which are considered in the relevant chapter of the EIAR.

(1) Prior to commencing floating track construction movement monitoring posts will be installed in areas where the peat depth is greater than 2m.

(2) Prior to any upgrading works, peat probing and hand shear vane testing will be undertaken along the route of the track.

(3) Base geogrid will be laid directly onto the existing peat surface along the line of the track in accordance with geogrid provider's requirements.

(4) The make-up of the new floated access track will be an average of 800mm of selected granular fill with 2 no. layers of geogrid with possibly the inclusion of a geotextile separator (drawing P24-234-0600-0005).

(5) Granular fill to be placed and compacted in layers in accordance with the TII Specification for Road Works, Series 600 (2024).

(6) The finished trackwidth will be approximately 4m, with wider sections on bends.

(7) Stone delivered to the floating track construction will be end-tipped onto the constructed floating track. Direct tipping of stone onto the peat will not be carried out.

(8) To avoid excessive impact loading on the peat due to concentrated end-tipping all stone delivered to the floating track will be tipped over at least a 10m length of constructed floating road.

(9) Where it is not possible to end-tip over a 10m length of constructed floating road then dumpers delivering stone to the floating track will carry a reduced stone load (not greater than half full) until such time as end-tipping can be carried out over a 10m length of constructed floating road.

(10) Following end-tipping suitable machinery will be employed to spread and place the tipped stone over the base geogrid along the line of the track.

(11) A final surface layer will be placed over the full width of the floating track, as per design requirements, and graded to accommodate wind turbine construction and delivery traffic.

# 4. EXCAVATIONS IN PEAT FOR TURBINE BASES, HARDSTANDINGS AND INFRASTRUCTURE FOUNDATIONS

The turbine bases will be founded on competent founding strata which will require excavation through peat and any soft subsoils. Only one turbine base (T7) remains to be excavated.

Similarly, crane hardstandings, blade storage areas, crane support pads and met mast foundations are to be founded on competent mineral soil which will also require excavation through peat and spoil. This excavation work will be undertaken from the existing hardstands to avoid any loading of the in-situ peat. Excavation for the borrow pit will also require the removal of peat and non-peat spoil overlying the rock.

## 4.1 Methodology

This methodology includes procedures that will be included in the construction to minimise any adverse impact on peat stability. The methodology is not intended to cover all aspects of construction such as drainage and environmental considerations, which are covered in Chapter 4 and 9 of the EIAR.

(1) With respect to placement of arisings from excavations the commitments given in Section 4 are to be followed. All excavated peat and spoil to be stored in appropriately designed locations, such as within the existing borrow pits and the proposed extension to the borrow pit. No material will be sidecast on the peat slopes.

(2) All excavations within peat will be adequately supported through the use of a stone cofferdam around the perimeter of the T7 hardstand. This will involve the excavation of peat in a trench and the backfill with crushed rock from the borrow pit, which will provide support to the in-situ peat. Excavation will commence on the northern side of the hardstand, from the existing berm, and progress along the western side of the hardstand.

(3) Excavations will be kept reasonably free from water at all times. Water will be prevented from being impounded within excavations by either using drainage channels cut into the excavation face or by pumping.

(4) Where water is channelled or pumped from an excavation then this water will be fed into an established watercourse or drainage ditch following suitable treatment, as described in Chapter 9 of the EIAR.

## 4.2 Supervision

All construction on the Wind Farm Site will be managed and controlled by the construction management team to ensure that all activities have been appropriately assessed with respect to peat stability and related health and safety. Procedures will be put in place to clearly demonstrate how this has been achieved, for example:

(1) Procedures that provide an auditable chain of command will be put in place to clearly demonstrate that peat stability and related health and safety have been assessed in the construction management.

(2) For any construction activity where peat stability and related health and safety have been assessed, then a permit to work will be issued to the construction operative by the appropriate personnel.

(3) No construction works will be started until a permit to work has been issued to the construction operative by the appropriate personnel.

(4) All works that may affect the stability of the Wind Farm Site will be routinely inspected and supervised on Wind Farm Site by appropriate personnel. Regular geotechnical inspection of the works associated with the Prospective Development will be undertaken by a suitably experienced geotechnical engineer.

(5) The above procedure will be independently audited by a suitably competent and experienced person(s). The competent person will have suitable professional qualifications and have experience of carrying out similar roles for construction projects in peatland.

(6) All persons involved in the assessment of peat stability on the Wind Farm Site will have sufficient expertise, competency, and experience for the tasks to which they have been assigned.

## 4.3 Weather Conditions

Restrictions will be enforced on work during or after periods of heavy or sustained rainfall as recorded from weather station located on the Wind Farm Site, or from Met Eireann weather forecasts. Heavy intense rainfall can result in degradation of the works resulting in localised instability, and in extreme cases can trigger large-scale peat failure.

(1) Following periods of heavy intense rainfall, such as 10mm/hr, >25mm in a 24-hour period, or >100% of monthly average in a 7-day period and in following 24 hours, no groundworks may take place and any ongoing works should be restricted to hardstanding areas.

(2) When periods of heavy intense rainfall are predicted then works will be ceased in advance and any construction works in critical areas with respect to stability are secured in advance.

(3) Following periods of heavy intense rainfall, the Wind Farm Site will be inspected prior to resumption of construction works by a competent person to ensure that all drainage is working, and critical areas with respect to stability are stable with no signs of ground movement.

# 5. EXCAVATION AND MANAGEMENT OF PEAT AND SPOIL

## 5.1 Excavation and Management of Arisings Methodology

This methodology includes procedures that are to be included in the construction phase to minimise any adverse impact on peat stability. The methodology is not intended to cover all aspects of construction such as drainage and environmental considerations, described in Chapter 4 and 9 of the EIAR.

(1) All excavated peat and spoil will be transported immediately on excavation to the designated peat management areas (see Drawing P24-234-0602-0001). No material is to be sidecast or stored on the in-situ peat on either side of the access roads/hardstands.

(2) Further details on the construction and reinstatement of the borrow pit and management areas are given in Section 4.5.

(3) Some of the peat, in particular the acrotelm (upper layer of the peat), excavated during construction will be used for landscaping purposes around the turbine bases, hardstands and underground cabling corridor.

(4) Sufficient space has been identified across the Wind Farm Site for the volume of peat and spoil that will be excavated as part of the Prospective Development.

## 5.2 Summary of Peat and Spoil Volumes on Site

A summary of the excavated peat and spoil volumes calculated for the Prospective Development is given in Table 5.1.

**Table 5.1: Summary of Excavated Peat and Spoil Volumes on Site**

| Infrastructure Element [1] | Proposed Dimensions | Peat Volume ($m^3$) [2] | Spoil (non-peat) Volume ($m^3$) [2] and [3] | Comment |
|---|---|---|---|---|
| Turbines and Hardstands | 27m diameter excavation footprint for turbine foundation with 50 x 30m hardstand area. | 29,100 | 500 | Hardstanding area and foundation footprint. Allowance included for mini-crane pads and blade finger hardstands associated with the main hardstand. |
| Access Roads | Assumed 5m running surface with 6-8m wide development footprint. | 27,300 | - | Allowance includes for widening on bends, at junctions, laybys, and tie-ins to hardstands. |
| Borrow Pits | | 14,700 | 1,500 | Stripping of peat/spoil |
| Berm at T01/T02 | | 3,900 | 500 | |
| Temporary Compounds | | 1,350 | | |
| Amenity Area | | 250 | | |
| | | | | |
| | **Total =** | **76,600$m^3$** | **2,500$m^3$** | **Total = 79,100$m^3$ (peat and spoil volume)** |

Note (1) The location of the infrastructure elements on the Wind Farm Site are shown on Drawing P24-234-0602-0001.

Note (2) Tree felling and stump flipping is proposed at various locations within the BMEP Site, however the proposed access track at this location is a floated track and as such this does not affect the excavation volumes, as no stump flipping will be undertaken below the footprint of the floating track.

Note (3) It should be noted that the excavated rock volume to be from the borrow pit is not included in the total volume quoted above in Table 5.1. It is assumed that the excavated rock volume will be re-used as part of the construction works for the Prospective Development and hence will not require reinstatement on the Wind Farm Site.

## 5.3 Summary of Peat and Spoil Management Areas on Site

A summary of the proposed peat and spoil management areas across the Wind Farm Site are given in Table 5.2.

**Table 5.2: Summary of Peat and Spoil Management Areas on Site**

| Location (1) | Peat and Spoil Volume ($m^3$) | Comment |
|---|---|---|
| Peat Cell at T18 | 8,700 | Backfilling of prepared peat cell. |
| Existing Borrow Pit (BP1) | 31,700 | Backfilling of existing excavation in bedrock. |
| Existing Borrow Pit (BP2) | 5,500 | Backfilling of existing excavation in bedrock. |
| Borrow Pit (BP3) | 99,500 | See Drawing P24-234-0602-0006 for further details. The material to be placed in the borrow pit will be a mixture of peat and spoil. |
| Landscaping (2) | 4,600 | Landscaping around the development footprint including the cabling corridor adjacent to the roads |
| | | |
| **Total =** | **150,000$m^3$** | |

Note (1) The location of the proposed borrow pits at the Wind Farm Site are shown on Drawing P24-234-0602-0001.

Note (2) Some of the acrotelm (upper layer of the peat) excavated during construction will be used for landscaping purposes.

## 5.4 Summary of Stone Volume Requirements

Table 5.3 below summarises the stone volume requirement for the Prospective Development, excluding the final blinding layer, comprising a 150mm layer of UGM-A (Clause 804).

**Table 5.3: Summary of Stone Volume Requirements**

| Infrastructure Element | Typical Dimensions | Stone Volume ($m^3$) (1) | Comment |
|---|---|---|---|
| Turbines and Hardstands | 27m diameter excavation footprint for turbine foundation with 50 x 30m finished hardstand surface. | 25,950 | Hardstanding area and foundation footprint. Allowance included for mini-crane pads and blade finger hardstands associated with the main hardstand, plus allowance for side slopes in areas of fill. |
| Access Roads (including cabling) | Assumed 5m running surface with 6-8m wide development footprint. Typical stone depth of 0.3-0.5m. | 33,350 | Allowance includes for widening on bends, at junctions, laybys, and tie-ins to hardstands. |
| Meteorological Mast | 12.5 x 14.5m hardstanding area. | 280 | - |
| Berm at road to T01/T02 | | 5,500 | |
| T04 floating road replacement | | 5,000 | Floating road section on approach to T4 to be removed and replaced with solid founded road. |
| T7 Access Road | | 1,700 | Removal of existing floated road section - floating road to be upgraded to solid founded road. |
| Floating Forestry Access Track to BMEP Site | 3m running width with 4m footprint | 2,400 | Includes upgrade of section of existing floating road and turning head. |
| | | | |
| | **Total =** | **74,180$m^3$** | |

Note (1) A contingency factor of 10% has been applied to the volumes to allow for expected bulking upon excavation and to allow for a variation in ground conditions across the Wind Farm Site.

## 5.5 Construction and Reinstatement of Borrow Pit

The location of the existing borrow pits is shown on Drawing P24-234-0602-0001, with the locations being: southwest of T12 (BP1), southeast of T15 (BP2) and adjacent to T13/T16 (BP3). Continued use and/or extension of excavation works at these locations are proposed as part of the Prospective Development The peat depth within the development footprint of the borrow pit extension (BP3) ranges from 0.6 to 3.0m. BP1 and BP2 will continue to be worked, however the footprint of the borrow pits will not be extended, and as such these will not generate any additional peat/spoil to be managed. Bedrock (Psammite) will be excavated, processed and used across the Site as granular fill for roads and hardstands.

Upon removal of the rock from within the borrow pits, it is proposed to reinstate the borrow pits using excavated peat and spoil. The excavated rock from the borrow pits will be used in the construction of the

infrastructure elements (turbine bases, roads, etc.) at the Wind Farm Site. The Contractor will be required to develop the borrow pits in a way which will allow the excavated peat and spoil to be placed safely. It is proposed to construct cells within the borrow pit (BP3) for the placement of the excavated peat and spoil. This is to allow for the safe placement and grading of the peat and spoil using dumper trucks and excavators. It also eliminates the need to construct above ground retaining structures which may have an unnecessary visual impact and increase the development footprint of the proposed wind farm. The text below provides design and construction commitments for the borrow pits.

It should be noted that there are significant excavation works required in order to develop the extension to the existing borrow pit (BP3) at the Wind Farm Site. Excavation works will be undertaken and supervised by an experienced contractor and the Project Geotechnical Engineer. The text below provides design and construction guidelines for the borrow pit.

Drawings P24-234-0602-0006 to 0008 show plan and cross sections of the borrow pits.

The borrow pit will be constructed as follows:

(1) Peat and overburden will be removed and stored within the void at the existing borrow pits. The rock within the proposed borrow pit footprint will be removed by breaking and blasting.

(2) It is proposed to construct the borrow pits so that the base of the borrow pits are below the level of the adjacent section of access road.

(3) Slopes within the excavated rock formed around the perimeter of the borrow pits will be formed at stable inclinations to suit local in-situ rock conditions. Exposed sections of the rock slopes will be left with irregular faces and declivities to promote re-vegetation and provide a naturalistic appearance.

(4) The stability of the rock faces within the borrow pits will be inspected by the Project Geotechnical Engineer upon excavation to ensure stability during construction works and in the long term. This inspection will allow unfavourable rock conditions to be identified and suitable mitigation measures to be applied such as removal of loose rock, in line with best practice guidelines.

(5) It will be necessary to construct rock buttresses within BP3 to create individual cells (up to 3 no. as required). The cells will be opened in sequence and filled as needed.

(6) A rock buttress to form cells with the borrow pit will be required to ensure access for trucks and excavators can be achieved. This will be formed by leaving in place an upstand of intact rock as the borrow pit excavation is progressed. See Drawing P24-234-0602-0006 for the location of the rock buttress. The location of the rock buttress shown on Drawing P24-234-0602-0006 for the borrow pit is indicative only and may change subject to local conditions encountered on the Wind Farm Site during construction. The rock buttress will be wide enough (up to 4m) to allow construction traffic access for tipping and grading during the placement of the excavated peat and spoil. The permanent side slopes of the internal rock buttress will be constructed at 45 degrees.

(7) Infilling of the peat and spoil will commence at the back edge of the borrow pit and progress towards the borrow pit entrance/rock buttress. The contractor excavating the rock will be required to develop the borrow pit in a way which will allow the excavated peat and spoil to be reinstated safely.

(8) The use of temporary access ramps and long reach excavators during the placement of the excavated peat and spoil will be required.

(9) The surface of the placed peat and spoil will be shaped to allow efficient run-off of surface water from the placed arisings towards the perimeter of the borrow pit.

(10) An interceptor drain will also be installed around the perimeter of the borrow pit. This drain will divert any surface water away from the borrow pit and hence prevent water from ponding and lodging during construction, and also when reinstated.

(11) Temporary control of groundwater within the borrow pit will be required. A temporary pump and suitable outfall locations will be required during construction.

(12) A settlement pond will be constructed at the lower side/outfall location of the borrow pit and is shown on the drainage drawings.

(13) The acrotelm will be placed with the vegetation part of the sod facing the right way up (where practicable) to encourage growth of plants and vegetation at the surface of the peat and spoil within the borrow pit.

(14) Supervision by the Project Geotechnical Engineer is required for the development of the borrow pit.

(15) All the above-mentioned requirements will be implemented by the Contractor during construction.

## 5.6 Peat Cell (T18)

A peat cell is proposed adjacent to T18, within an existing worked area. The location of this is shown on drawing P24-234-0602-0001 and a plan and cross section is shown in drawing P24-234-0602-0009.

(1) The placement of peat within the peat cell will require the use of long reach excavators.

(2) The surface of the placed peat will be shaped to allow efficient run-off of surface water. Shaping of the surface of the peat/spoil will be carried out as placement of peat within the peat cell progresses. This will reduce the likelihood of debris run-off and reduce the risk of instability of the placed peat.

(3) The acrotelm will be placed on the finished surface with the vegetation part of the sod facing the right way up (where practicable) to encourage growth of plants and vegetation at the surface of the placed peat and spoil within the placement areas.

(4) Supervision by the Project Geotechnical Engineer is required for the development of the peat cell.

# 6. GENERAL COMMITMENTS FOR GOOD CONSTRUCTION PRACTICE

To minimise the risk of construction activity causing potential peat instability the Construction Method Statements (CMS) for the Prospective Works will also implement, but not be limited to, the general measures below together with the specific measures.

(1) Uncontrolled concentrated water discharge onto peat slopes identified as being unsuitable for such discharge will be avoided. All water discharged from excavations during work will be piped over areas specifically assessed as being unsuitable and hence directly into suitable drainage lines.

(2) All excavations will be suitably supported to prevent collapse and development of tension cracks.

(3) Installation and regular monitoring of geotechnical instrumentation during construction in areas of poor ground, such as deeper peat deposits (see Section 7).

(4) Ground conditions to be assessed by suitably experienced geotechnical engineer.

(5) Regular briefing of all site staff (e.g. toolbox talks) to provide feedback on construction and ground performance and to promote reporting of any observed change in ground conditions.

(6) Routine inspection of the Wind Farm Site by the Contractor and Project Geotechnical Engineer will be undertaken and will include an assessment of ground stability conditions (e.g. cracking, excessive floating road settlement, disrupted surface, closed-up drains) and drainage conditions (e.g. blocked drains, absence of water in previously flowing drains, springs, etc).

# 7. INSTRUMENTATION

## 7.1 Movement Monitoring Posts

To monitor possible peat movements, it is proposed to install sighting posts upslope and downslope of areas where excavations will be undertaken, and where floating roads will be upgraded, such as along the floating access roads to T01-T04, and upslope and downslope of T07, the upgraded access road to T18 and the upgraded and new floated forestry access track to the BMEP Site. Further details of monitoring locations are given in the FT Geotechnical & Peat Stability Assessment Report for the Prospective Development (FT, 2026).

Details of sighting posts are given below.

(1) A line of sighting posts will comprise:

  (a) A line of wooden stakes (typically 1 to 1.5m long) placed vertically into the peat to form a straight line.

  (b) The sighting line will comprise 6 no. posts at 5m centres that is a line some 25m long.

  (c) A string line will be attached to the first and last posts and all intervening posts will be adjusted so they are just touching the string line.

(2) Lines of sighting posts will be placed across the existing slope about 5m away from the area to be worked. The posts will be located along the road at 10m intervals in areas of deeper peat (greater than 2.0m). Where there are relatively steeper slopes or softer ground a sighting line will be placed down the slope, or at any location where monitoring is deemed necessary by the Project Geotechnical Engineer.

(3) Each line of sighting posts will be uniquely referenced with each post in the line given a reference. The post reference will be marked on each post (e.g. reference 1-1, 1-2, 1-3, 1-4, 1-5, 1-6 for posts in line 1).

(4) The sighting lines will be monitored at the beginning of each working day, and during the day where considered appropriate (e.g. when working activity is concentrated at a specific location).

(5) Monitoring of the posts will comprise sighting along the line and recording any relative movement of posts from the string line.

(6) Where increased movements are recorded the frequency of monitoring will be increased.

(7) A monitoring record will be kept of the date, time and relative movement of each post, if any. This record will be updated and stored as a spreadsheet.

## 7.2 Post-Construction Monitoring

To monitor possible peat movements following the construction of the Prospective Development, it is recommended that the Wind Farm Site is inspected by a suitably qualified engineer annually for the first three years following commissioning of the Prospective Development. Particular attention should be given to the floating roads, as well to any areas where the site drainage is not functioning as intended.

# 8. CONTINGENCY MEASURES

## 8.1 Excessive Movement

Where there is excessive movement or continuing peat movement recorded at a monitoring location or identified at any location within the Wind Farm Site but no apparent signs of distress to the peat (e.g. cracking, surface rippling) then the following will be carried out.

(1) All activities (if any) will cease within the affected area.

(2) Increased monitoring at the location will be carried out. The area will be monitored until such time as movements have ceased.

(3) Re-commencement of activities will only start following a cessation of movement and agreement with all parties (Contractor/Engineer/Designer).

## 8.2 Onset of Peat Slide

In the unlikely event where there is the onset or actual detachment of peat (e.g. cracking, surface rippling) then the following will be carried out.

(1) On alert of a peat slide incident, all activities (if any) in the area will cease and all available resources will be diverted to assist in the required mitigation procedures.

(2) Action will be taken to prevent a peat slide reaching any watercourse. This will take the form of the construction of check barrages on land. Due to the terrain, the possible short run-out length to watercourses, speed of movement and the inability to predict locations it may not be possible to implement any on land prevention measures, in this case a watercourse check barrage will be implemented.

(3) All relevant authorities (such as Donegal County Council) will be notified if a peat slide event occurs on the Wind Farm Site.

(4) For localised peat slides that do not represent a risk to a watercourse and have essentially come to rest the area will be stabilised initially by rock infill, if required. The failed area and surrounding area will then be assessed by the engineering staff and stabilisation procedures implemented. The area will be monitored, as appropriate, until such time as movements have ceased.

## 8.3 Check Barrages

Whilst it is not anticipated based on the analysis undertaken that a peat slide will occur on Wind Farm Site, as a contingency a check barrage procedure is included below.

The check barrage procedure deals with preventing a peat slide from moving downstream within a watercourse.

The most effective method of preventing excessive peat slide debris from travelling downstream in a watercourse is the use of a check barrage. A check barrage comprises the placement of rock fill across a watercourse. The check barrage is a highly permeable construction that will allow the passage of water but will prevent peat debris from passing through. Rock fill will comprise well-graded coarse rock pieces from about 200mm up to typically 5000mm.

The rock fill for any check barrage will be sourced from the borrow pit on the Wind Farm Site.

The size of the barrage will vary depending on the scale of the peat debris to be contained and the geometry of the watercourse at the barrage location. In general, due to the low speed of a peat slide there is generally little impact force and most of the lateral load is due to fluid pressure on the upslope face of the barrage.

The check barrage will fill the entire channel width of the watercourse up to a height of 3 to 4m with a crest width of typically 3m and side slopes of about 35-45 degrees depending on the geometry of the barrage location.

Rock will not be tipped directly into open excavation in an uncontrolled manner. Its placement will be controlled by excavator operator. No construction machinery will track onto in-situ peat. In the event that machinery must track onto peat the peat will be inspected and assessed by a competent person to avoid excessive loading. If in any doubt machinery will not be tracked onto peat.

The check barrage procedure is as follows:

(1) Access to the check barrage location will be along the existing access roads on the Wind Farm Site and/or along public roads, where possible. When it is necessary to form the barrage then rock fill will be placed across the watercourse to effectively block the passage of peat debris.

(2) Operatives employed to carry out the construction of the check barrage will be inducted by means of a briefing by on-site supervisors as to the proposed location of the check barrage.

(3) The check barrage provides containment for peat debris in the highly unlikely event of a major peat slide. Further remedial measures, should they be required, will be assessed by the Contractor and the Project Geotechnical Engineer, and carried out as soon as physically possible when the location and extent of the failure is established.

(4) Where a barrage was constructed as a precaution and no peat debris reached the watercourse then the barrage will be removed as soon as any measures to prevent further peat sliding are agreed with all parties (Contractor/Engineer/Designer).

# 9. REFERENCES

Fehily Timoney (2021). Meenbog Wind Farm – Assessment of Site with respect to Peat Stability.

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# DRAWINGS

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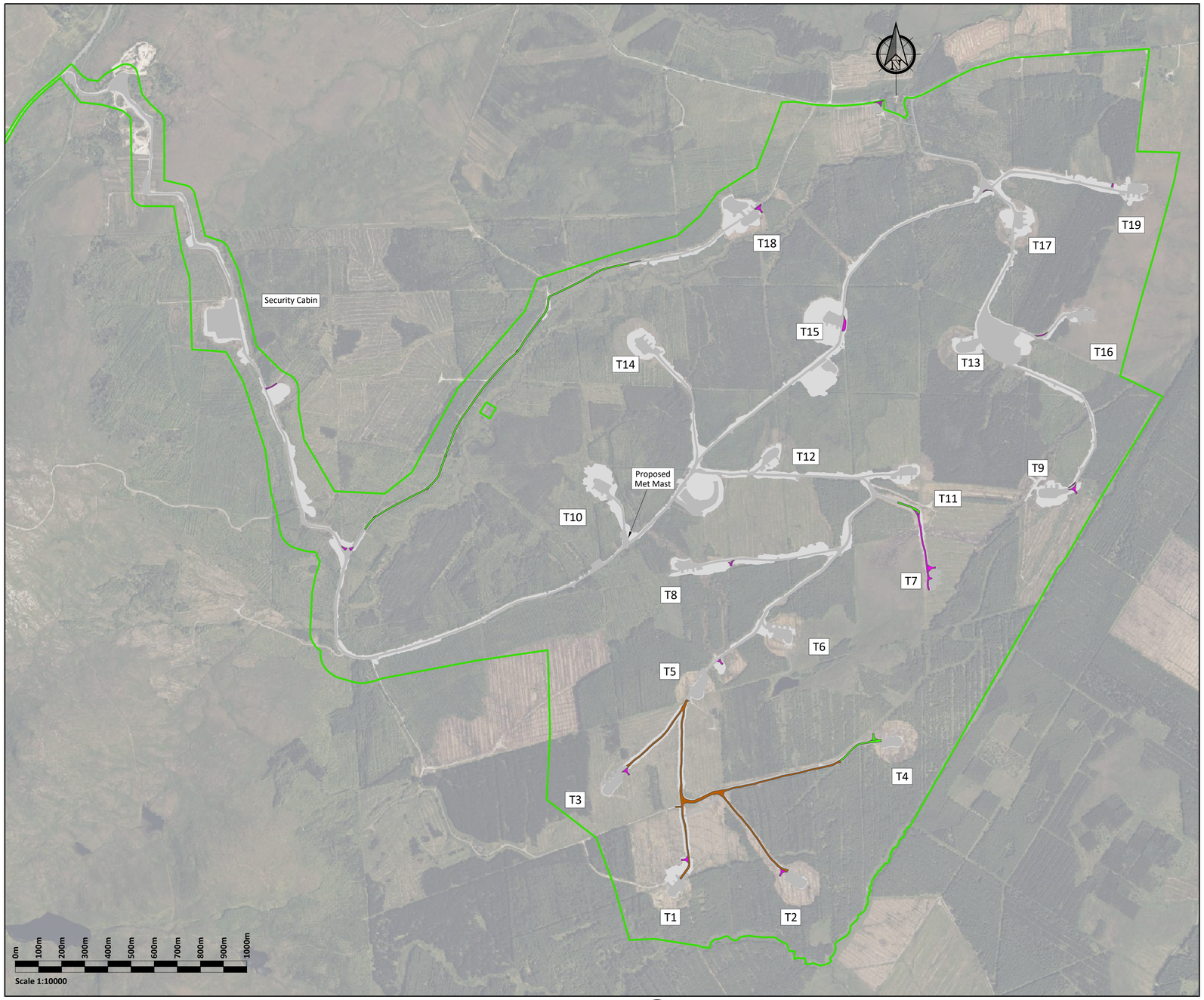


PLAN
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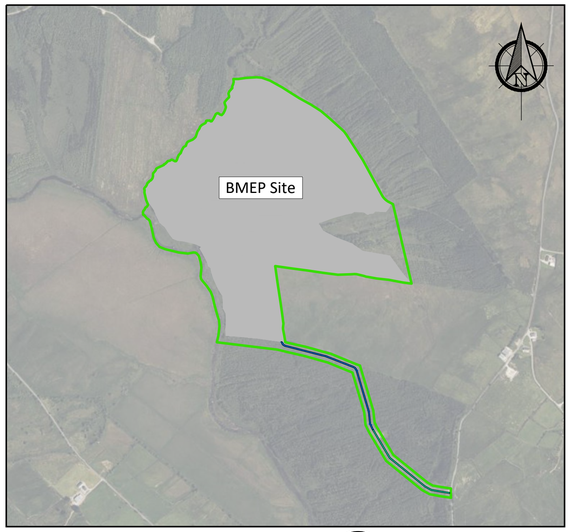
Plan Legend:

- Type A - Upgrade of Existing Founded Road
- Type B - Upgrade of Existing Floating Road to Founded
- Type B1 - Upgrade of Existing Floating Forestry Access Track
- Type C - Upgrade of Existing Floating Access Road
- Type D - New Floating Forestry Access Track
- Prospective Development
- Existing Development
- Site Boundary

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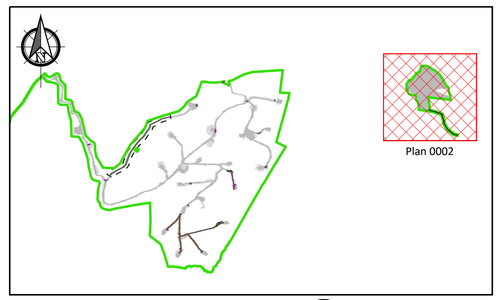


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PROJECT
**MEENBOG WIND FARM (PROSPECTIVE DEVELOPMENT)**

CLIENT
**MKO**

SHEET
**ROAD CONSTRUCTION TYPES PLAN**

Date: 07.04.26
Drawn by: POR
Checked by: IH
Project number: P24-234
Scale (@ A1 ): As Shown
Drawing Number: P24-234-0602-0001
*(Sheet set subset PSMP Prospective)*
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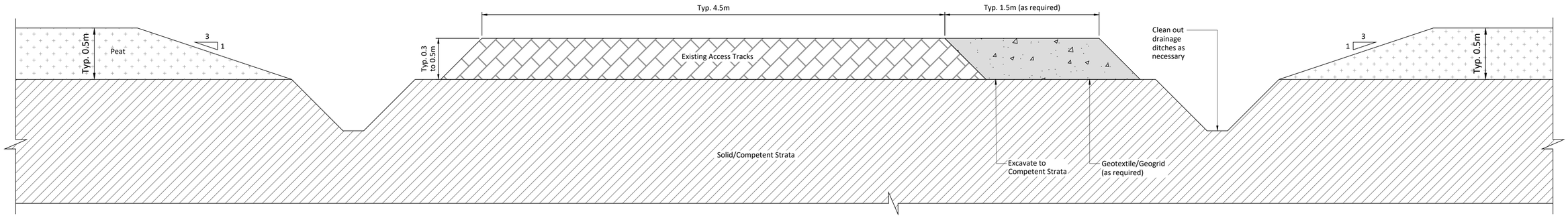


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| SHEET: TYPE A - UPGRADE OF EXISTING FOUNDED ACCESS ROAD | Date: 07.04.26 | Project number: P24-234 | Scale (@ A1 ): As Shown |
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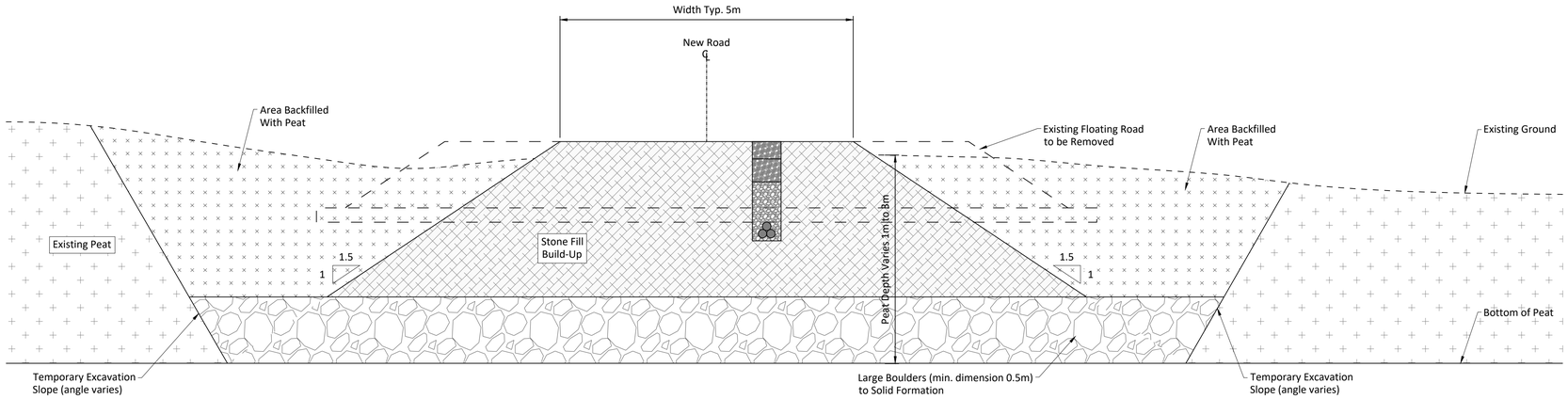


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PROJECT

**MEENBOG WIND FARM (PROSPECTIVE DEVELOPMENT)**

CLIENT

**MKO**

SHEET

**TYPE B - UPGRADE OF EXISTING FLOATING ACCESS TRACK TO FOUNDED ACCESS TRACK**

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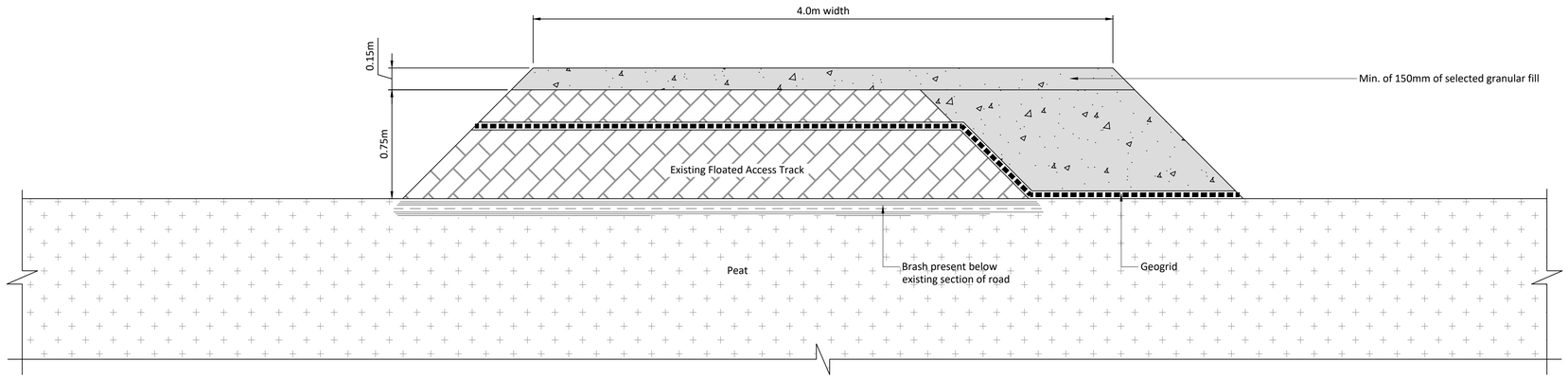


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PROJECT

MEENBOG WIND FARM
(PROSPECTIVE DEVELOPMENT)

CLIENT

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TYPE B1 - UPGRADE OF EXISTING FLOATED ACCESS ROAD

Date 07.04.26

Drawn by POR

Checked by IH

Project number P24-234

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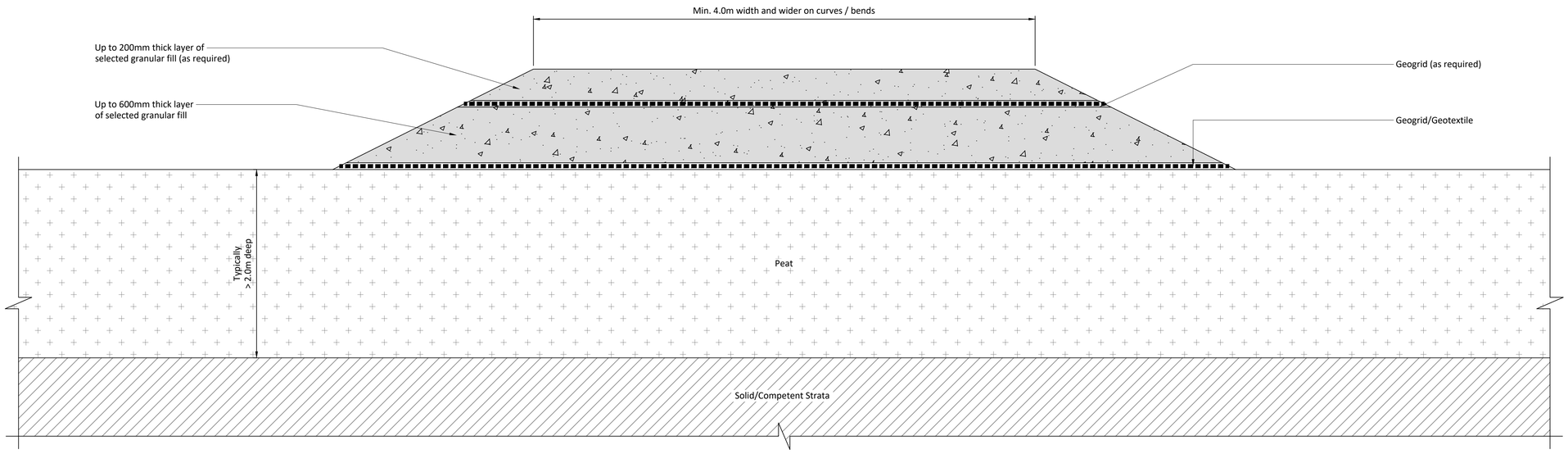


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PROJECT

MEENBOG WIND FARM
(PROSPECTIVE DEVELOPMENT)

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TYPE D - NEW FLOATED ACCESS TRACK

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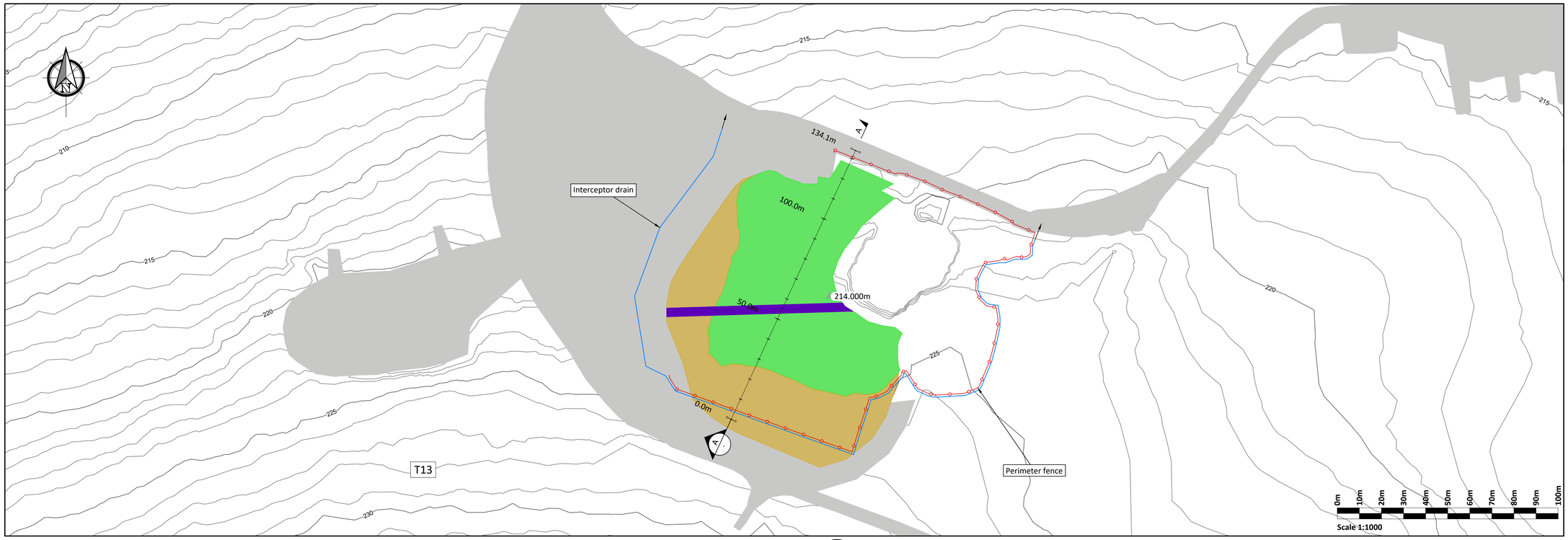


PLAN

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BP3

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## Plan Legend:

- Prospective Development
- Site Boundary
- Peat Cell
- Borrow Pit
- Extension to Borrow Pit
- In-Situ Rock Berm
- Proposed Borrow Pit Working Strip
- Proposed Fence
- Existing Ground Contour - Major
- Existing Ground Contour - Minor

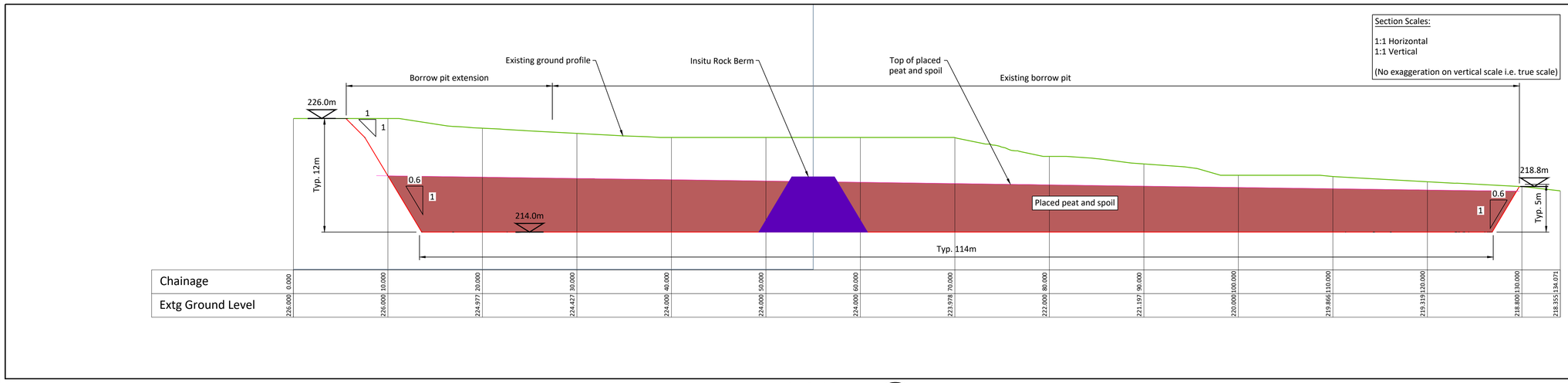
## Construction Notes Borrow Pit:

(1) Slopes within the excavated rock around the perimeter of the borrow pit will be formed at stable inclinations to suit local in-situ rock conditions.

(2) Infilling of the peat & spoil will commence at the back edge of the borrow pit and will progress towards the borrow pit entrance. An internal buttress will be constructed to allow the borrow pit to be developed and infilled in cells.

(3) The surface of the placed peat & spoil will be shaped to allow efficient run-off of surface water from the placed arising's.

(4) Further guidelines on the construction of the borrow pit are included within Section 5.5 of the Peat & Spoil Management Plan




SECTION

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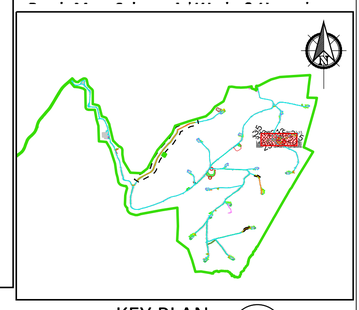

KEY PLAN

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| P01 | FOR INFORMATION | BDH | 07.04.26 |
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PROJECT

**MEENBOG WIND FARM (PROSPECTIVE DEVELOPMENT)**

CLIENT

**MKO**

SHEET

**EXTENSION TO EXISTING BORROW PIT 3**

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|---|---|---|---|
| Date 07.04.26 | Project number P24-234 | Scale (@ A1 ) As Shown | |
| Drawn by POR | Drawing Number P24-234-0602-0006 (Sheet set subset PSMP Prospective) | | Rev P01 |
| Checked by IH | | | |

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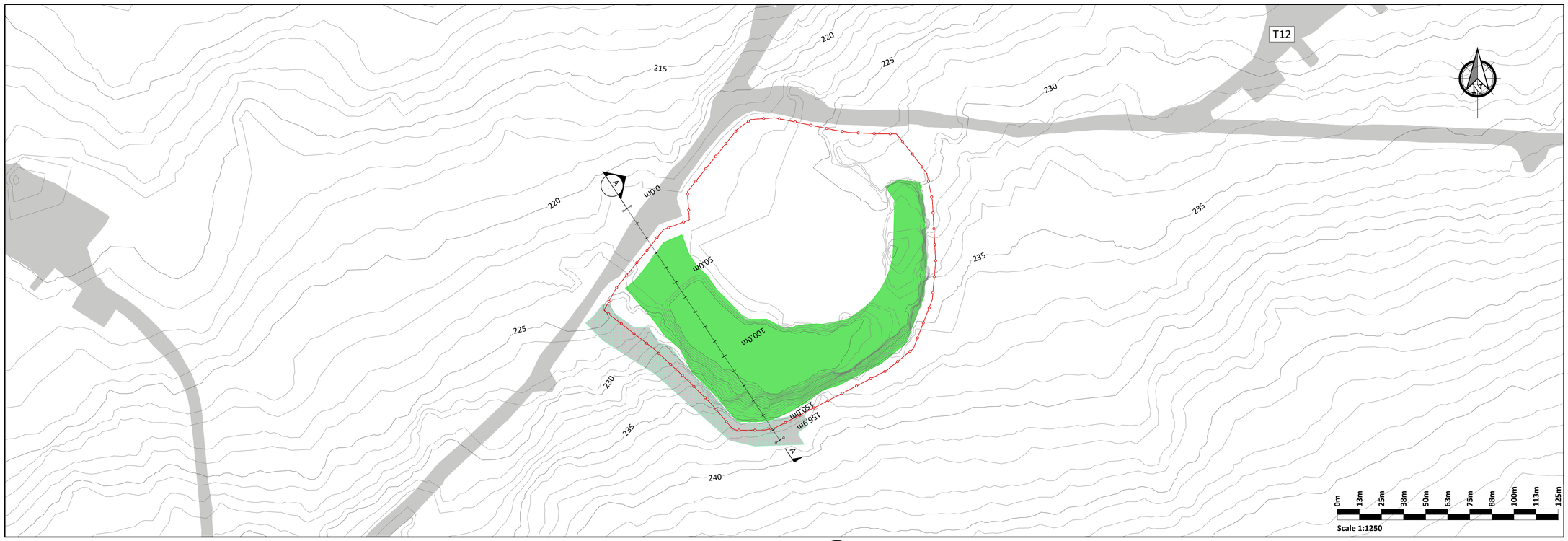
25 June 2026 (O:\ACAD\2024\P24-234\P24-234-0602-0006)




PLAN
1:1250
BP1
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## Plan Legend:

- Prospective Development
- Site Boundary
- Peat Cell
- Borrow Pit
- Extension to Borrow Pit
- Proposed Borrow Pit Working Strip
- Proposed Fence
- Existing Ground Contour - Major
- Existing Ground Contour - Minor

## Construction Notes:

(1) Prior to the placement of any excavated peat and spoil, the existing perimeter buttress is to be inspected and widened if necessary.

(2) The finished surface of the stored peat/spoil will be at least 0.5m below the top of the perimeter buttress.

(3) An interceptor drain should also be installed upslope of the peat cell.

(4) A silting pond will be required at the lower side of the peat cell.

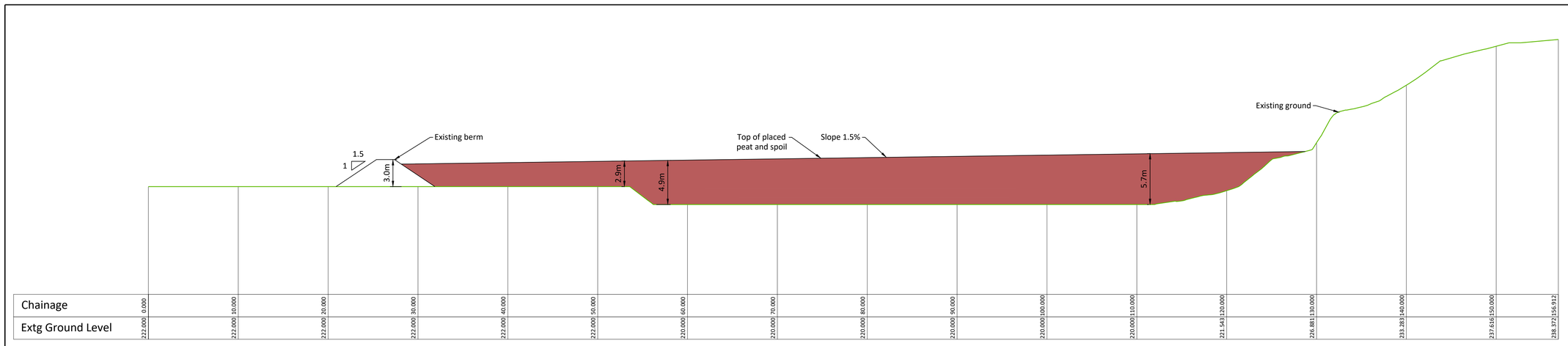
(5) The placement of the excavated spoil should commence at the back of the peat cell and work towards the perimeter buttress.

(6) It is important that the surface of the stored peat/spoil be shaped to allow efficient run-off of water from the stored peat/spoil.

(7) Supervision by a geotechnical engineer or appropriately competent person is recommended for the construction of the peat cell.

(8) All the above mentioned requirements should be confirmed by the designer prior to construction.

(9) Further guidelines on the construction of the peat cell are included within Section 5.5 of the Peat & Spoil Management Plan.




SECTION
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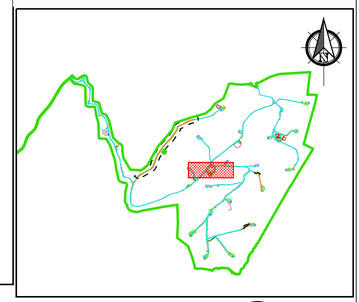


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PROJECT
**MEENBOG WIND FARM (PROSPECTIVE DEVELOPMENT)**

CLIENT
**MKO**

SHEET
**PEAT CELL (BP1)**

Date 07.04.26
Drawn by POR
Checked by IH
Project number P24-234
Scale (@ A1 ) As Shown
Drawing Number **P24-234-0602-0007**
*(Sheet set subset PSMP Prospective)*
Rev **P01**

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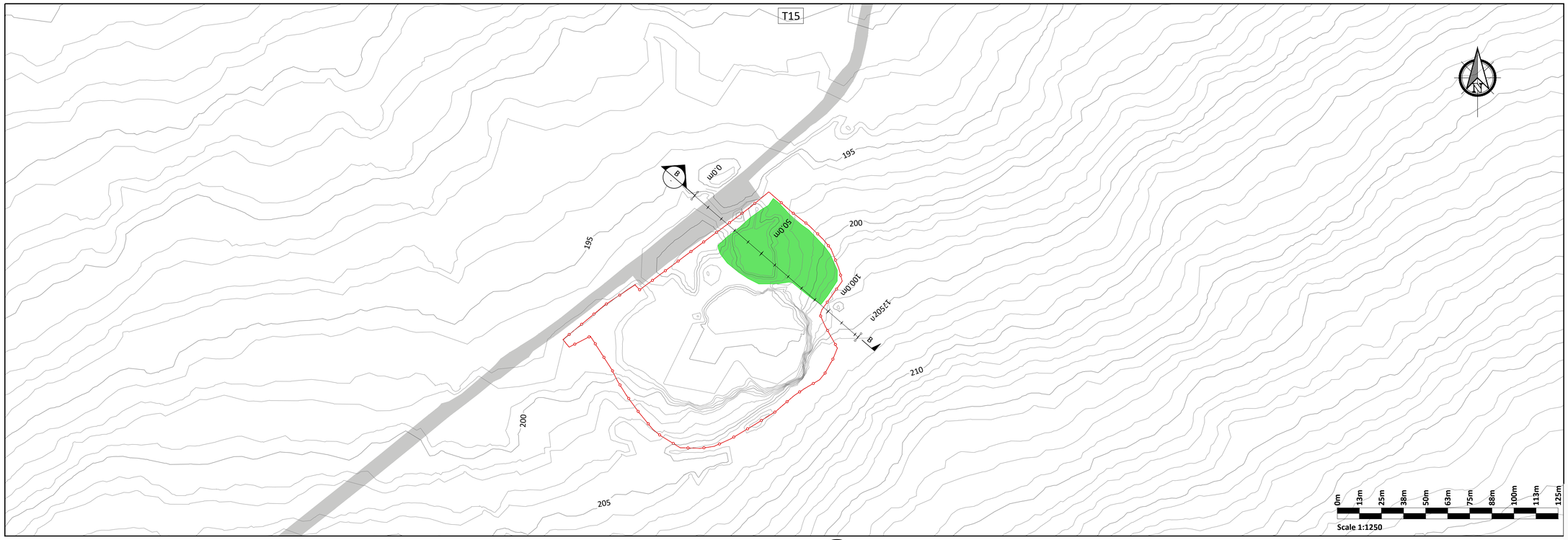
22 June 2026 (O:\ACAD\2024\P24-234\P24-234-0602-0007)




PLAN

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BP2

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## Plan Legend:

- Prospective Development
- Site Boundary
- Peat Cell
- Borrow Pit
- Extension to Borrow Pit
- Proposed Fence
- Existing Ground Contour - Major
- Existing Ground Contour - Minor

## Construction Notes:

(1) Prior to the placement of any excavated peat and spoil, the existing perimeter buttress is to be inspected and widened if necessary.

(2) The finished surface of the stored peat/spoil will be at least 0.5m below the top of the perimeter buttress.

(3) An interceptor drain should also be installed upslope of the peat cell.

(4) A silting pond will be required at the lower side of the peat cell.

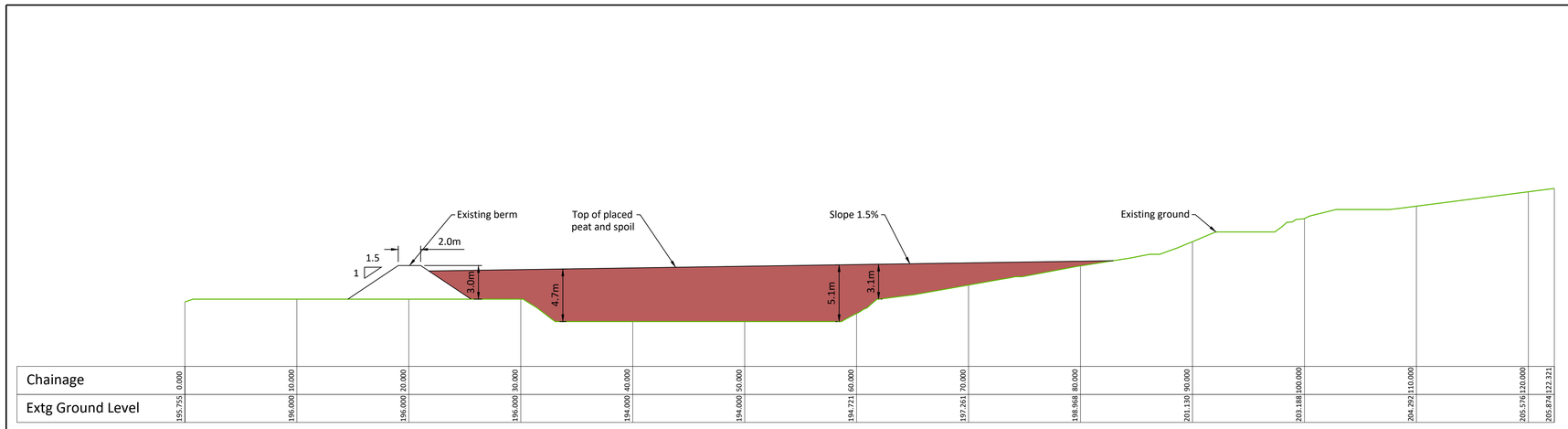
(5) The placement of the excavated spoil should commence at the back of the peat cell and work towards the perimeter buttress.

(6) It is important that the surface of the stored peat/spoil be shaped to allow efficient run-off of water from the stored peat/spoil.

(7) Supervision by a geotechnical engineer or appropriately competent person is recommended for the construction of the peat cell.

(8) All the above mentioned requirements should be confirmed by the designer prior to construction.

(9) Further guidelines on the construction of the peat cell are included within Section 5.5 of the Peat & Spoil Management Plan.




SECTION

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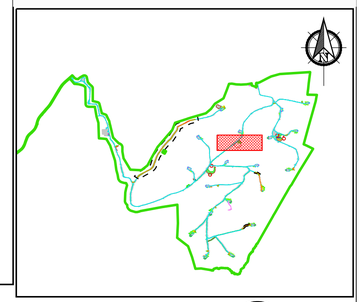


KEY PLAN

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| PROJECT | MEENBOG WIND FARM (PROSPECTIVE DEVELOPMENT) |
| CLIENT | MKO |
| SHEET | PEAT CELL (BP2) |
| Date | 07.04.26 |
| Drawn by | POR |
| Checked by | IH |
| Project number | P24-234 |
| Scale (@ A1 ) | As Shown |
| Drawing Number | P24-234-0602-0008 (Sheet set subset PSMP Prospective) |
| Rev | P01 |

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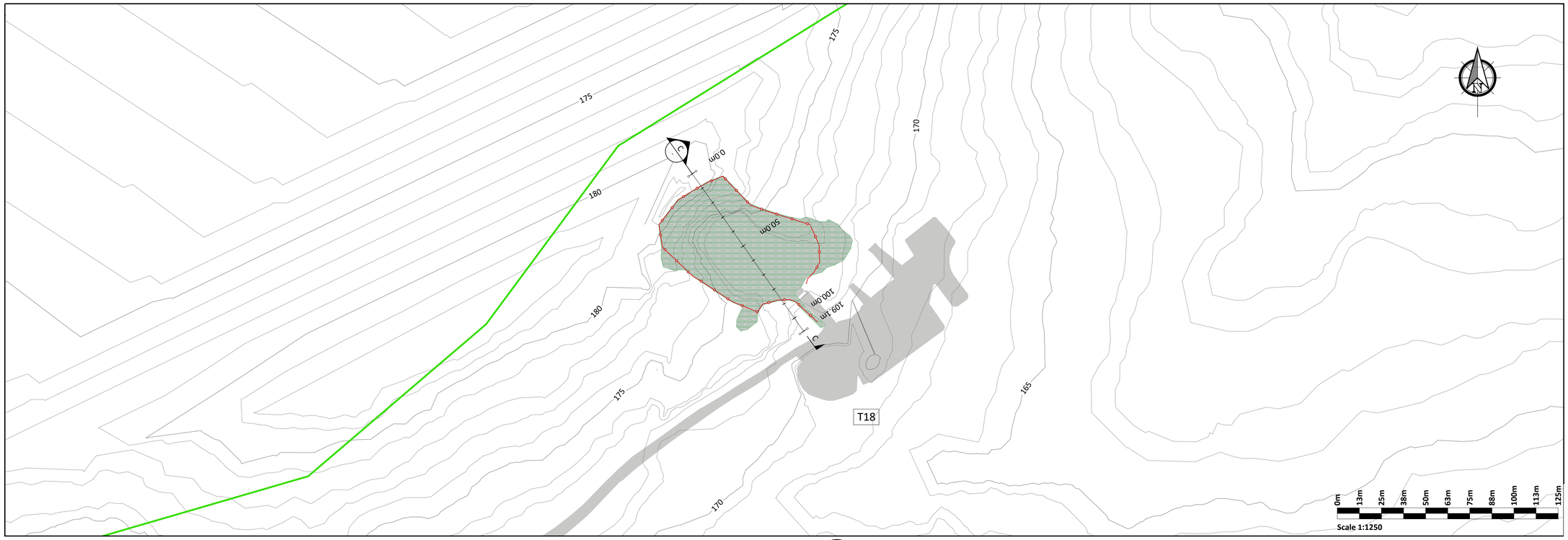


PLAN
1:1250
T18
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## Plan Legend:

- Prospective Development
- Site Boundary
- Peat Cell
- Proposed Fence
- Existing Ground Contour - Major
- Existing Ground Contour - Minor

## Construction Notes:

(1) The finished surface of the stored peat/spoil will be at least 0.5m below the top of the existing rock level at the entrance to the peat cell.

(2) An interceptor drain should also be installed upslope of the peat cell.

(3) A silting pond will be required at the lower side of the peat cell.

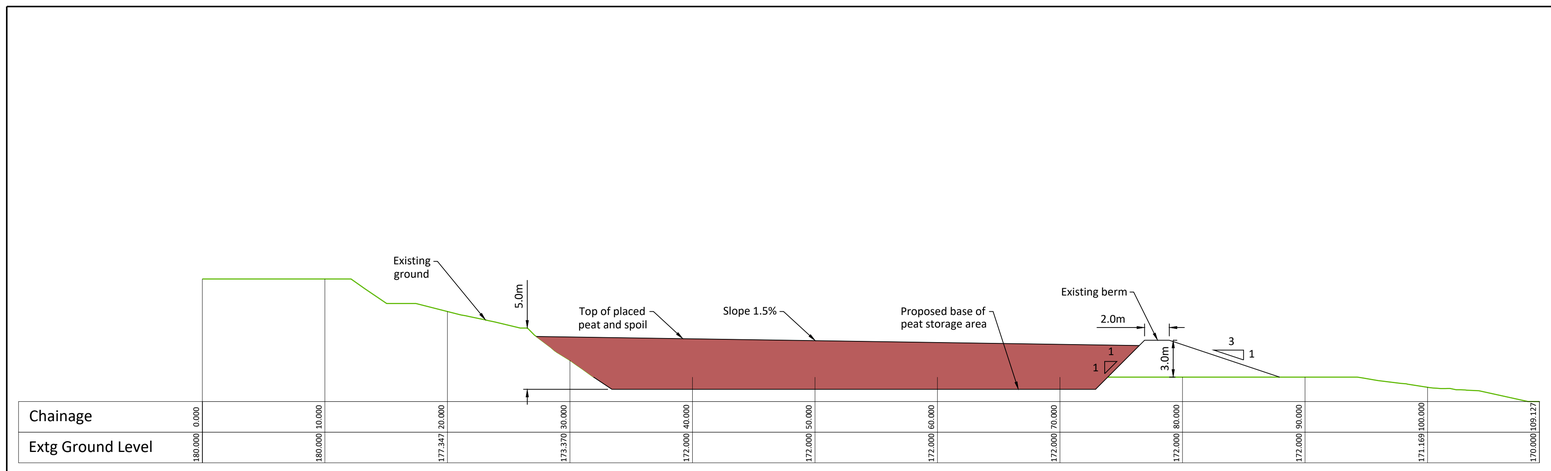
(4) The placement of the excavated spoil should commence at the back of the peat cell and work towards the entrance to the peat cell.

(5) It is important that the surface of the stored peat/spoil be shaped to allow efficient run-off of water from the stored peat/spoil.

(6) Supervision by a geotechnical engineer or appropriately competent person is recommended for the construction of the peat cell.

(7) All the above mentioned requirements should be confirmed by the designer prior to construction.

(8) Further guidelines on the construction of the peat cell are included within Section 5.6 of the Peat & Spoil Management Plan.




SECTION
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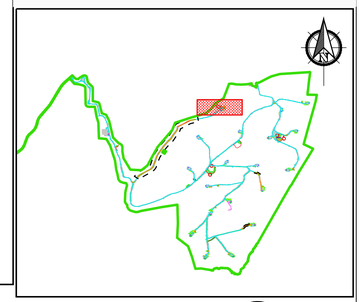


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| PROJECT | MEENBOG WIND FARM (PROSPECTIVE DEVELOPMENT) |
| CLIENT | MKO |
| SHEET | PEAT CELL (T18) |
| Date | 07.04.26 |
| Project number | P24-234 |
| Scale (@ A1 ) | As Shown |
| Drawn by | POR |
| Checked by | IH |
| Drawing Number | P24-234-0602-0009 |
| Rev | P01 |

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